

Bonded Repair of Composite Airframe Laminate and Sandwich Structures



John S. Tomblin, PhD
Lamia Salah
Dr Bill Stevenson



Curt Davies
FAA Technical Monitor



Michael Borgman (Spirit Aerosystems)
Robert Bohaty (Spirit Aerosystems)
Amador Motos (Adam Aircraft)



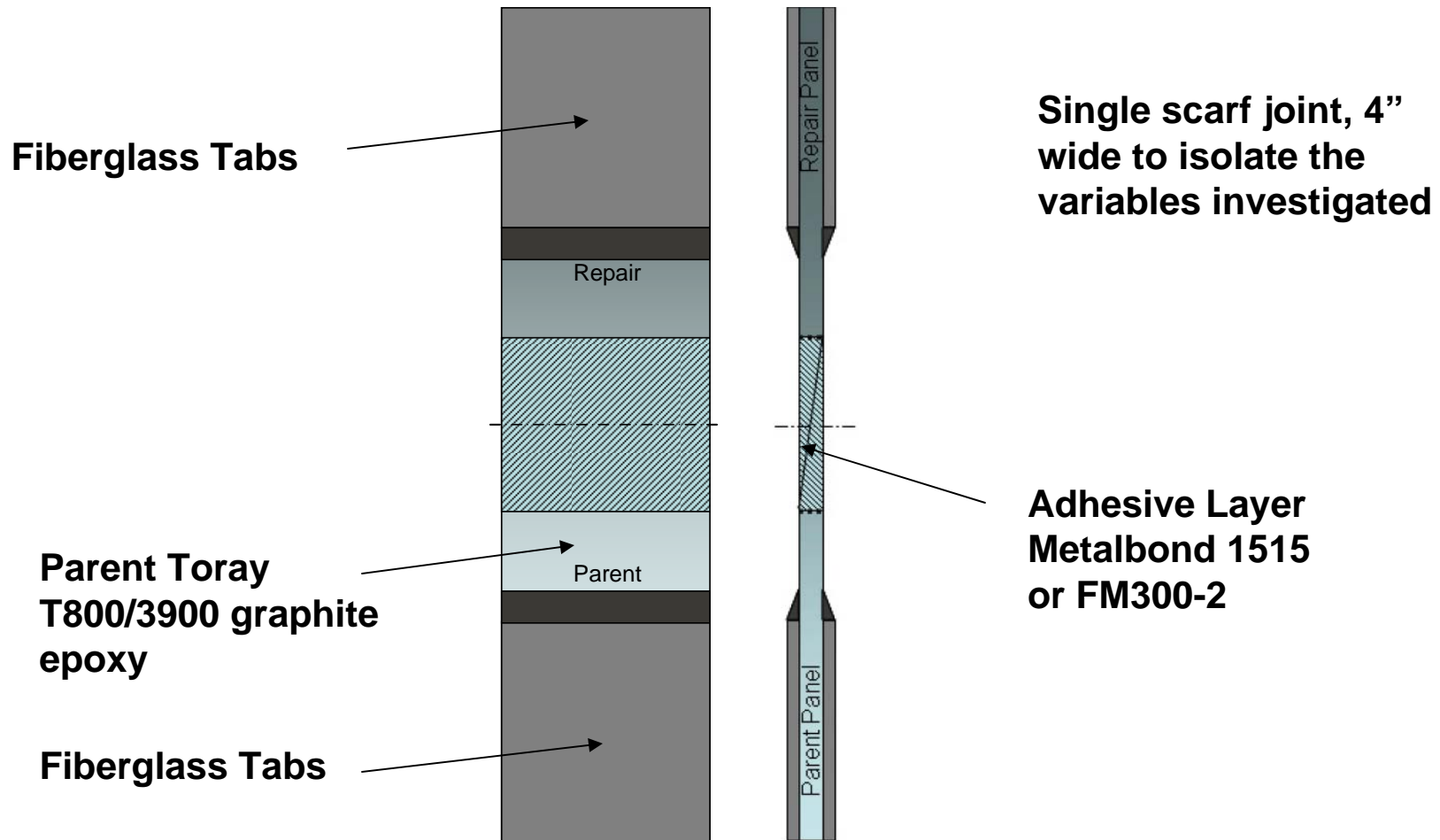
Presented at the CACRC meeting, November 16th 2007

Objective

To investigate different variables on the performance of repairs applied to solid laminates and sandwich structures

- **To generate baseline repair data (static and fatigue) for both laminate/ sandwich configurations using OEM/ Factory but also field repairs**
- **To evaluate the strength/ durability of poorly bonded and/or contaminated repairs that passed NDI (Laminate/Sandwich)**
- **To evaluate the damage tolerance of repairs subjected to BVID inflicted at three different locations on the repair (Laminate)**
- **To provide recommendations pertaining to process improvement to ensure repair bond repeatability and structural integrity**

Laminate Repair Coupon Configuration



Methodology

OEM Repair Material Evaluation

- To generate baseline repair data with the parent material (T800/3900) used as the repair material (OEM repair), 96 coupons used for the investigation

- 18, 32 ply
- Moduli
- Scarf rates
- Static/ fatigue performance

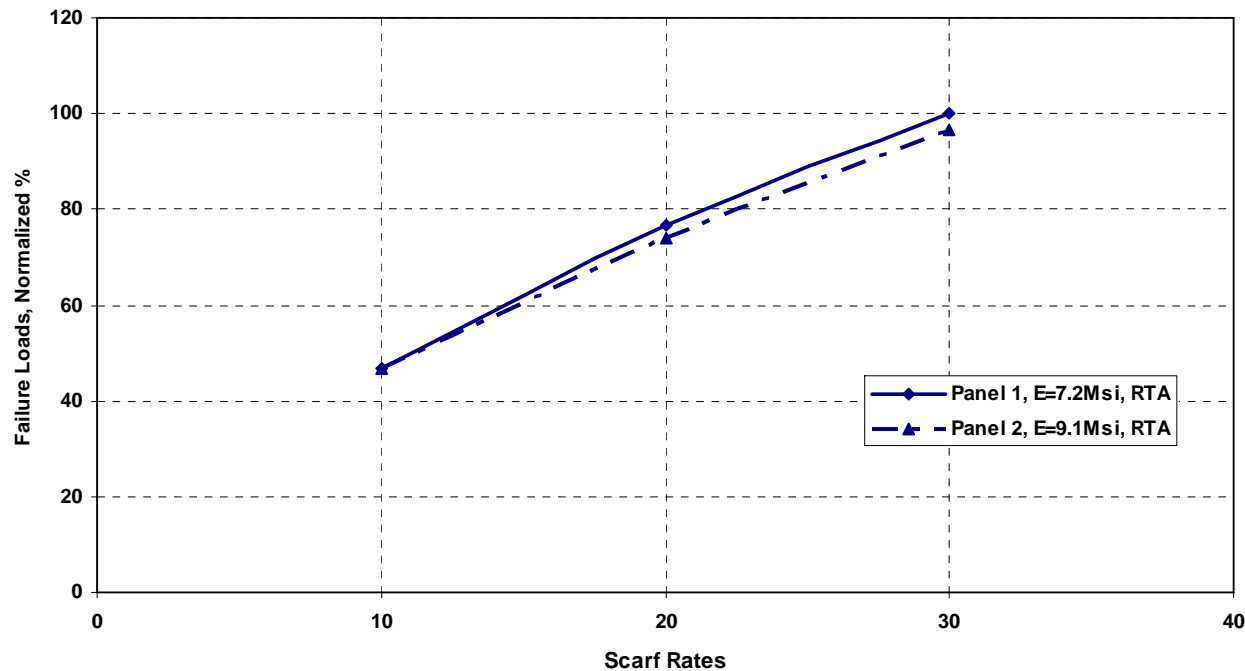
Panel #	Thickness (in)	E (Msi)	Scarf Rate	STATIC	FATIGUE
				RTA	RTA
1	0.1332	7.2	10	6	3
			20	6	3
			30	3	3
2	0.1332	9.1	10	6	3
			20	6	3
			30	3	3
3	0.2368	7.7	10	6	3
			20	6	3
			30	3	3
4	0.2368	8.8	10	6	3
			20	6	3
			30	3	3

Methodology

OEM Repair Material Evaluation- Results

100% corresponds to the failure load of the -30 repairs
increased load carrying capability with increased repair size
comparable performance for both panels

Failure Loads, normalized vs. Scarf Rates (Panels 1 & 2)



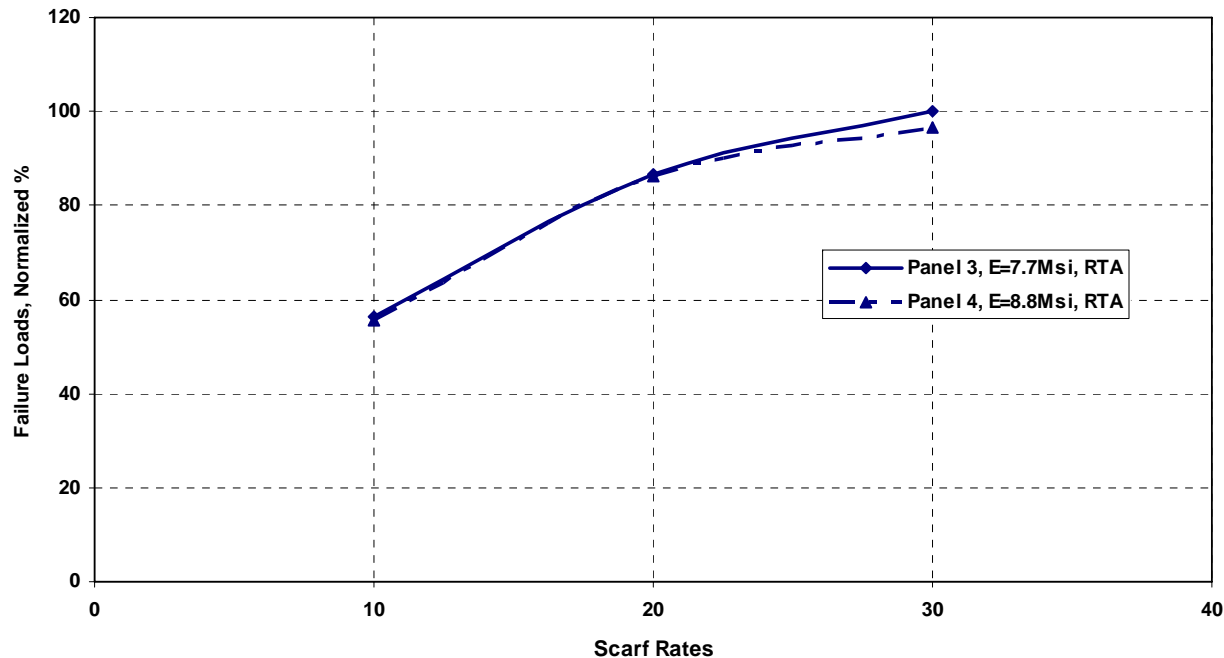
Methodology

OEM Repair Material Evaluation-Results

100% corresponds to the failure load of the -30 repairs

increased load carrying capability with increased repair size (32 ply)

Failure Loads, Normalized vs. Scarf Rates (Panels 3 & 4)

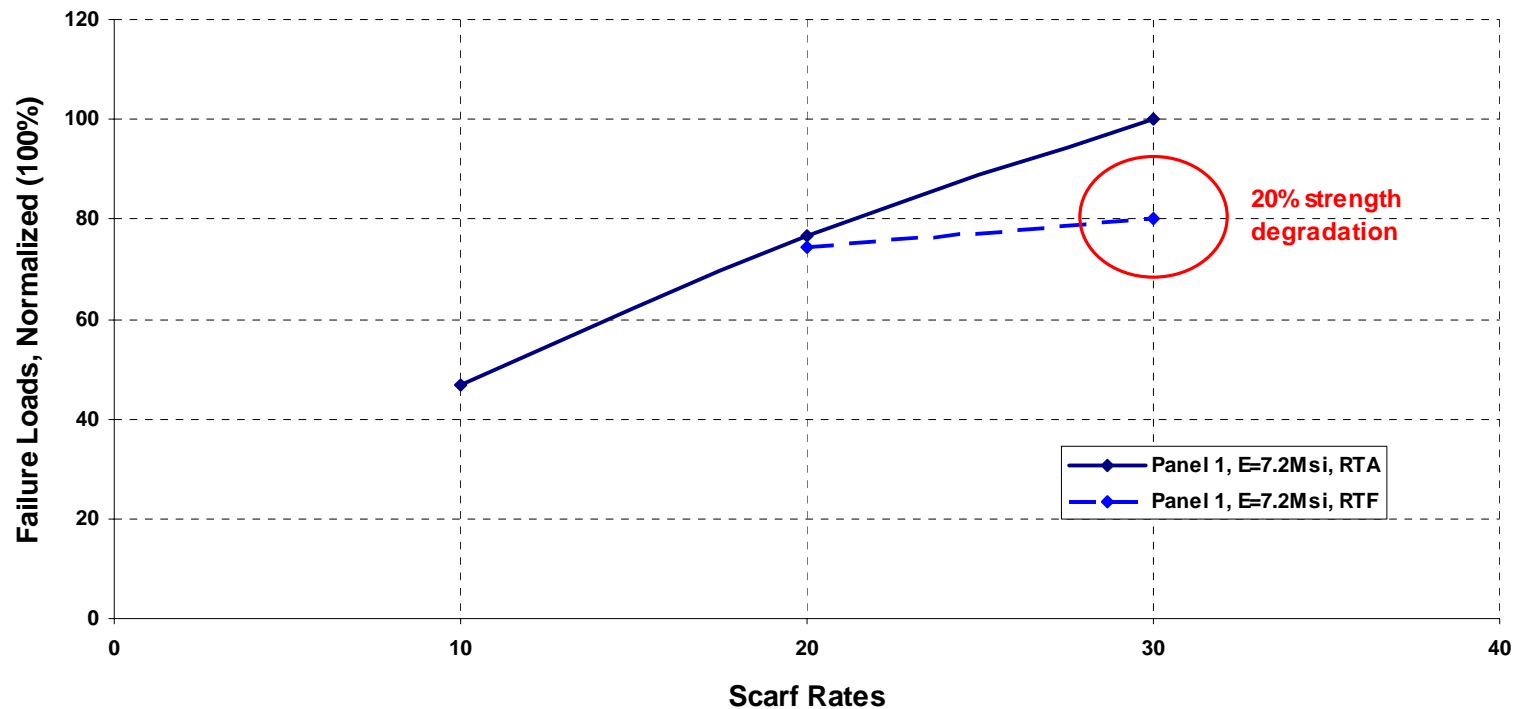


Methodology

OEM Repair Material Evaluation

100% corresponds to the failure load of the -30 repairs
comparison of the RS after fatigue to the static strength

Static/ Residual Strength vs. Scarf Rates (Panel 1)

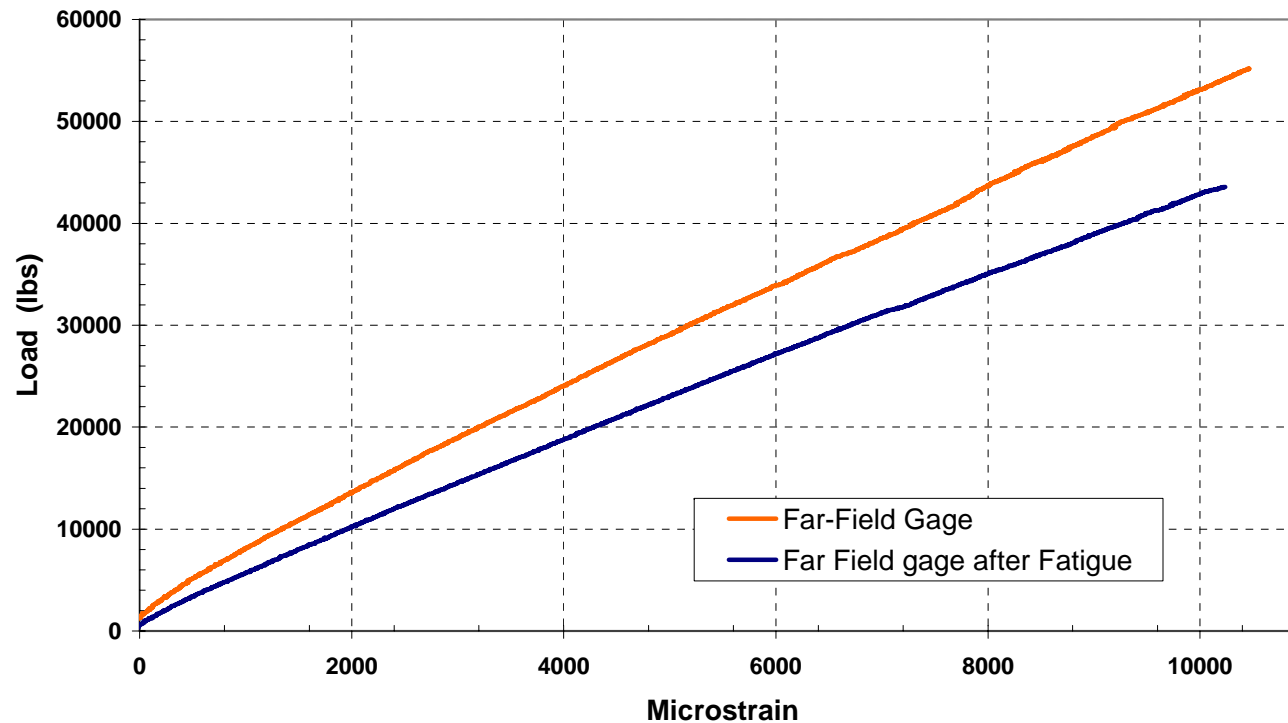


Methodology

OEM Repair Material Evaluation

Load vs strain for static and residual strength coupon
Stiffness loss after fatigue

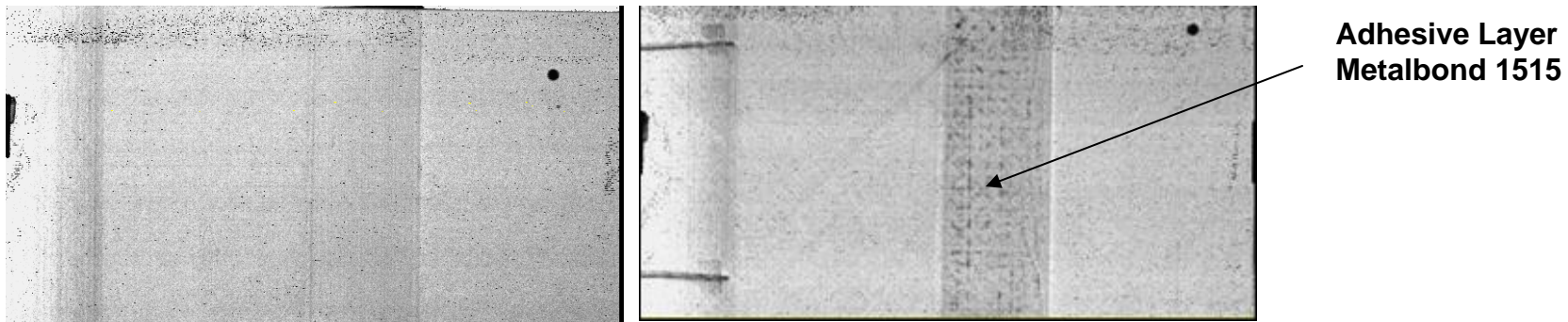
Load Versus Strain (1-1-30-RTA vs 1-1-30-RTF)



Methodology

OEM Repair Material Evaluation

- Bonded Repair performance is dependent on variability in repair process
- Overall increases in static performance with increased repair size
- Stiffer panels tend to have a lower strength capability than panels with lower stiffness (more pronounced poisson's effects)
- All -20 and -30 repairs survived 165000 cycles of fatigue at 3000 microstrain demonstrating acceptability of these repairs at that strain level
- The 18ply panels residual strength after fatigue was 20% lower than their ultimate static strength capability due to a change in compliance/ stiffness after fatigue (adhesive plastic deformation)



Methodology

Field Repair Material Evaluation

- To generate baseline repair data for a candidate field repair material (ACG T800/ MTM45-1, 250°F vacuum cure system), 72 coupons used for this investigation (scarf rates correspond to 5.7°, 2.86° and 1.98°)

- 18, 32 ply
- Moduli
- Scarf rates
- Static/ fatigue performance

Panel #	T (in)	E (Msi)	Scarf Rate	STATIC	FATIGUE
				RTA	RTA
1	0.1332	7.2	10	3	3
			20	3	3
			30	3	3
2	0.1332	9.1	10	3	3
			20	3	3
			30	3	3
3	0.2368	7.7	10	3	3
			20	3	3
			30	3	3
4	0.2368	8.8	10	3	3
			20	3	3
			30	3	3

Methodology

Field Repair Material Evaluation

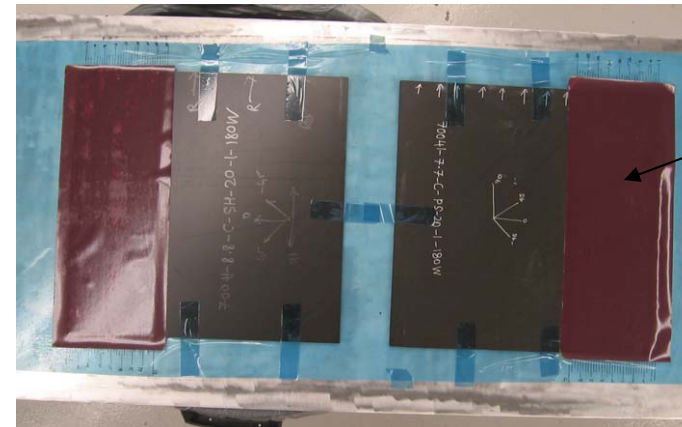
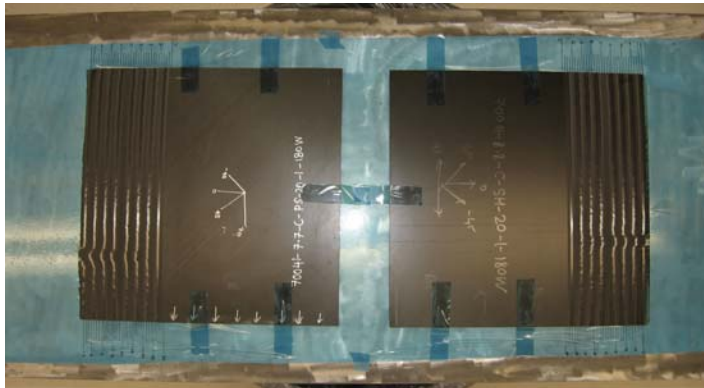
Panel preparation, Repair Procedure Details



Scarf Machining



Scarfed Panels



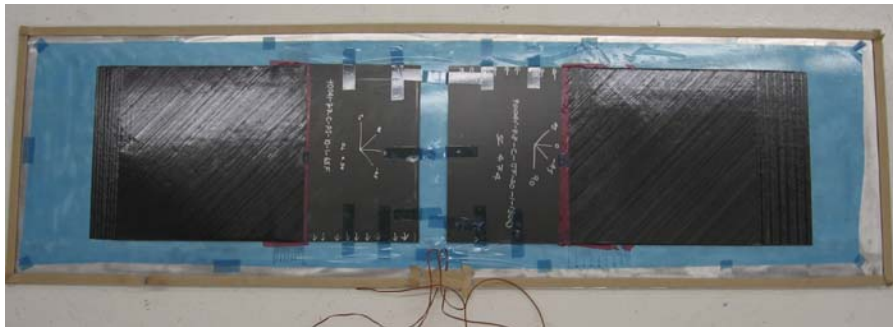
**Adhesive Layer
FM300-2**

Repair Implementation

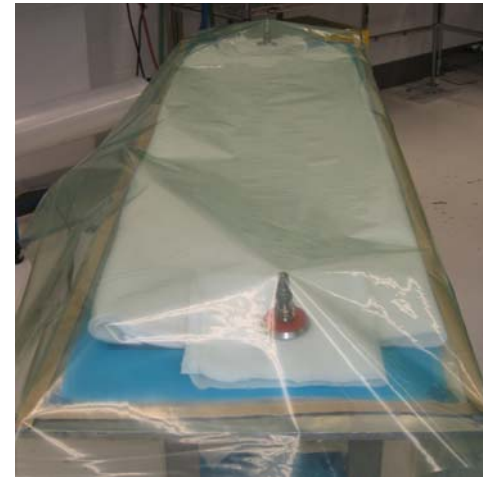
Methodology

Field Repair Material Evaluation

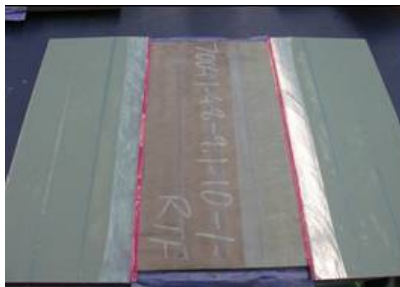
Repair ply lay-up following edge markings



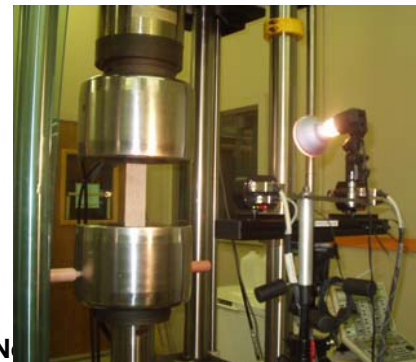
Repair Implementation



Repair Bagging/ Curing



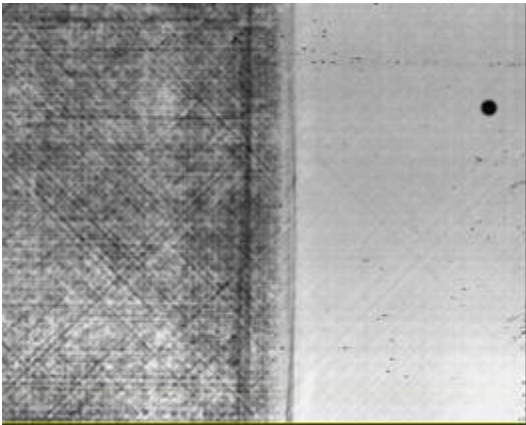
Tabbed Panel



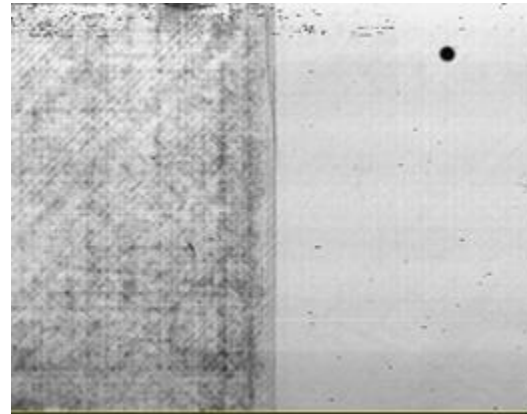
Mechanical Testing

Methodology

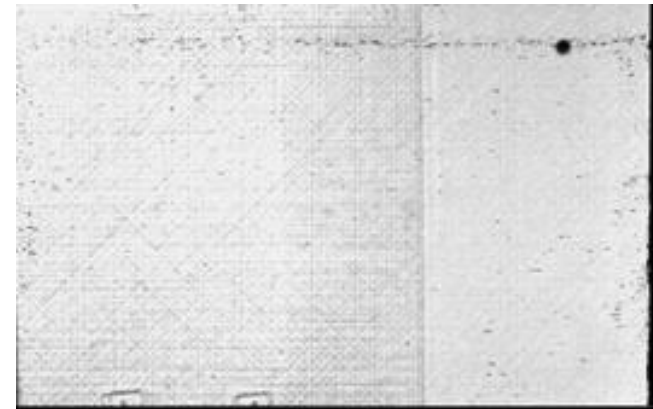
Field Repair Material Evaluation



ACG 2-1-10-RTA



ACG 2-1-10-RTF



4-2-20-RTA

- **Process yielded repairs with various levels of porosity as illustrated by the C-Scan images**
Possible source of variability in the mechanical data

Results

Field Repair Material Evaluation

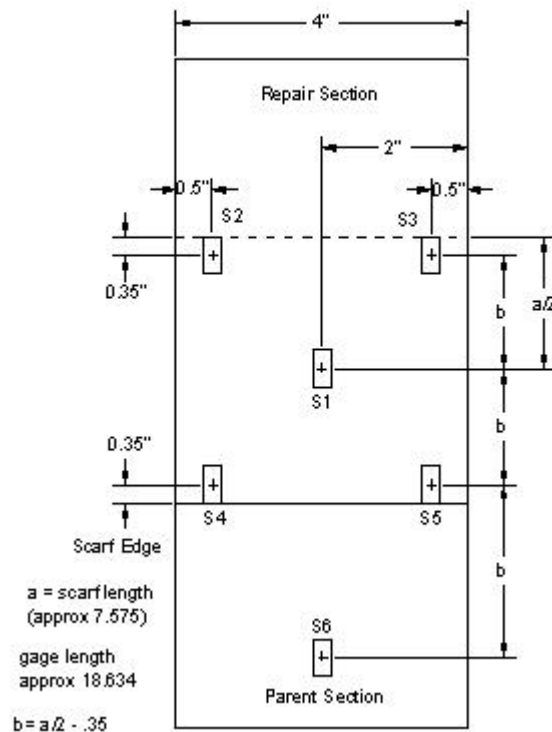
➤ ARAMIS

a non-contact optical 3-D deformation measuring system that uses two high resolution cameras to monitor strain concentrations in a test article

the test article is sprayed with a random pattern prior to loading

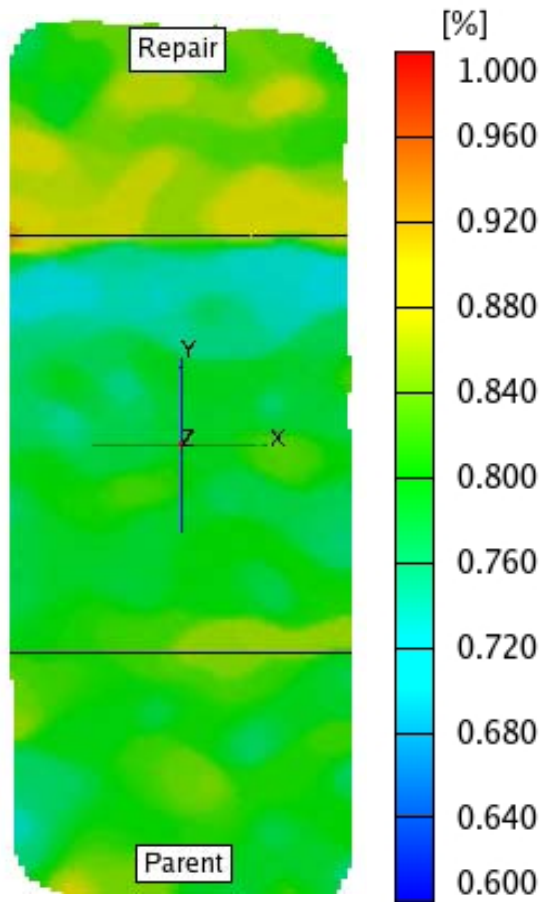
measurements are taken at different load levels,

changes in displacements and rotations between stages are recorded, from which strains can be calculated

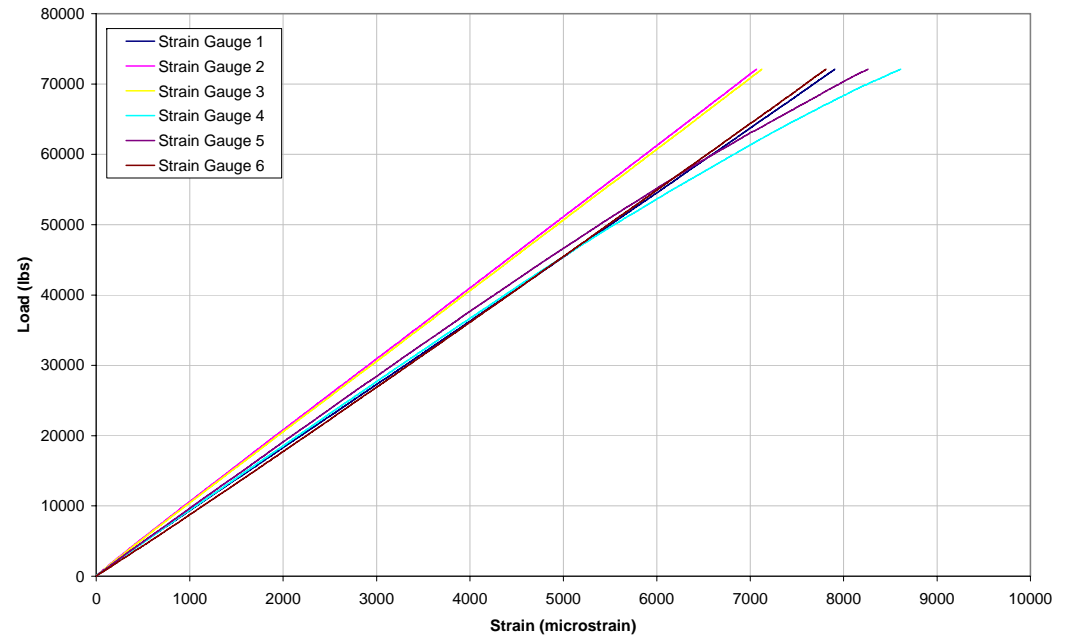


Results

Field Repair Material Evaluation



ACG-4-2-20-RTA-03



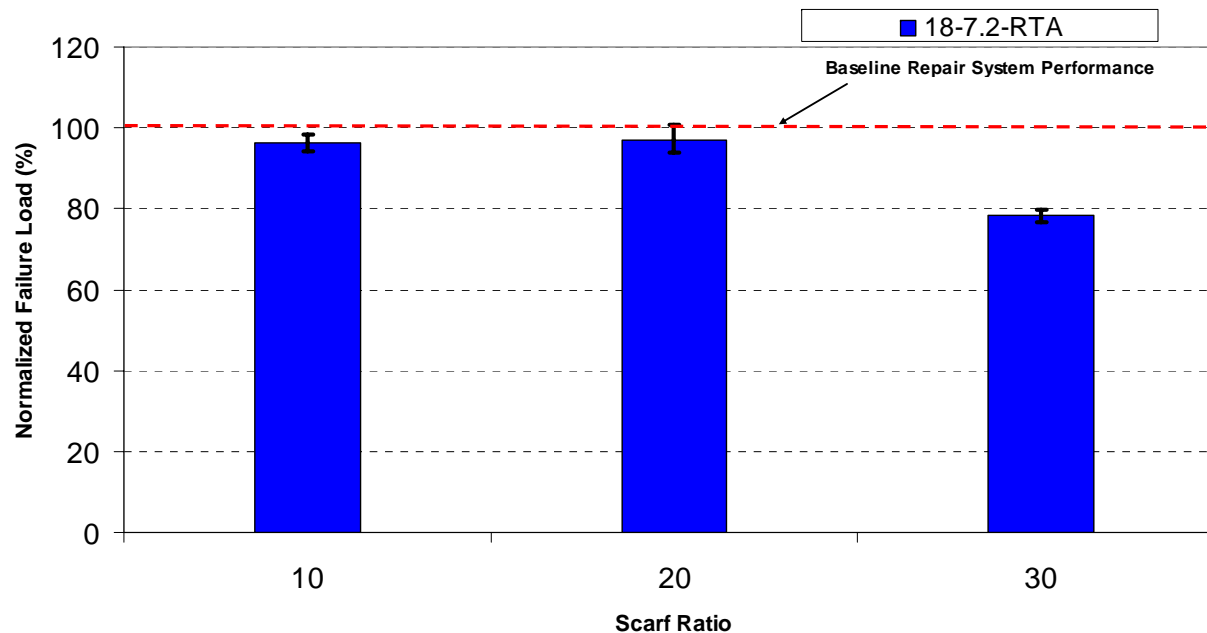
**Y-Strain Distribution for
ACG-4-2-20-RTA-01**

Results-Static

Field Repair Material Evaluation

- Comparison of static strength of the field repairs wrt OEM repairs
- 100% represents the failure load of the baseline repairs (parent material same as repair material)
- At least 80% “baseline repair performance” was restored at room temperature
- Variability (process, bondline thickness)

Field Repair Material Performance



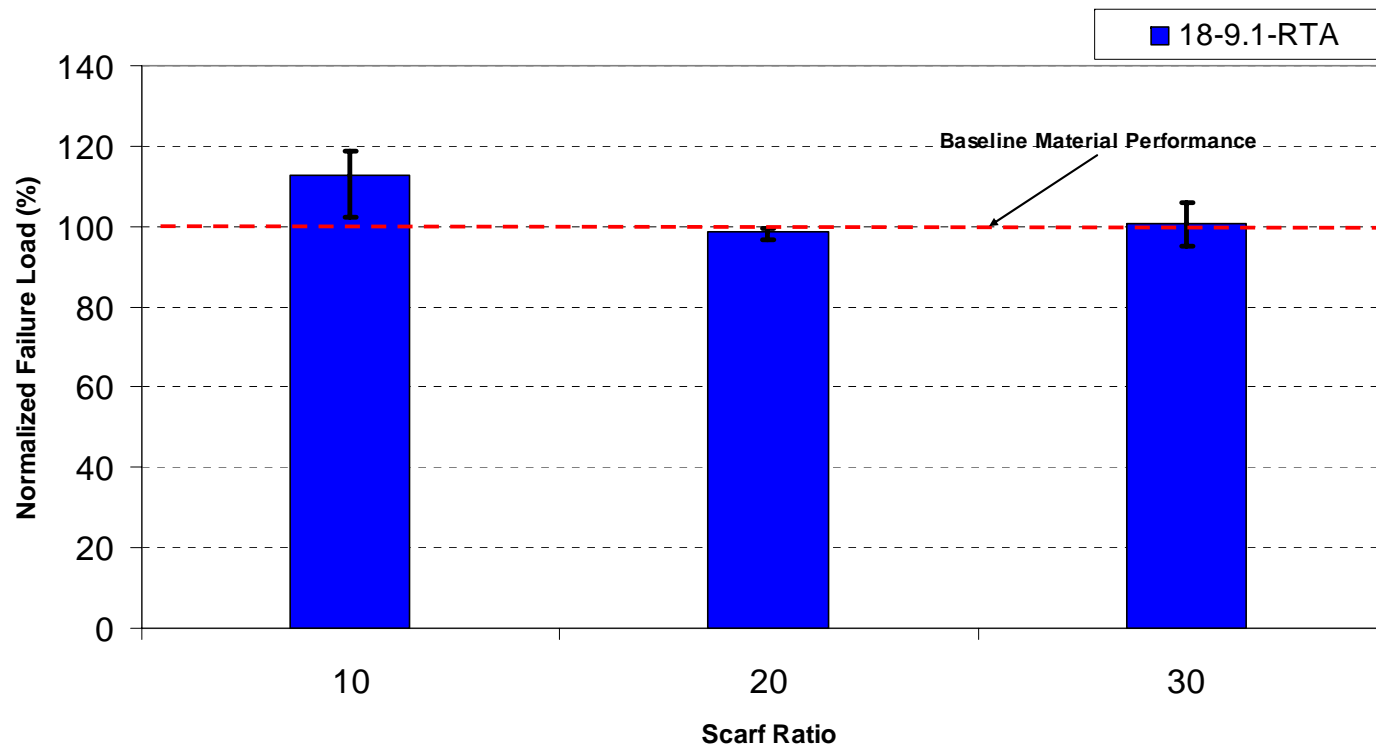
Presented at the CACRC Meeting, November 16th, 2007

Results-Static

Field Repair Material Evaluation

- Comparison of static strength of the field repairs wrt OEM repairs
- At least 98% “baseline repair performance” was restored at room temperature

Field Repair Material Performance

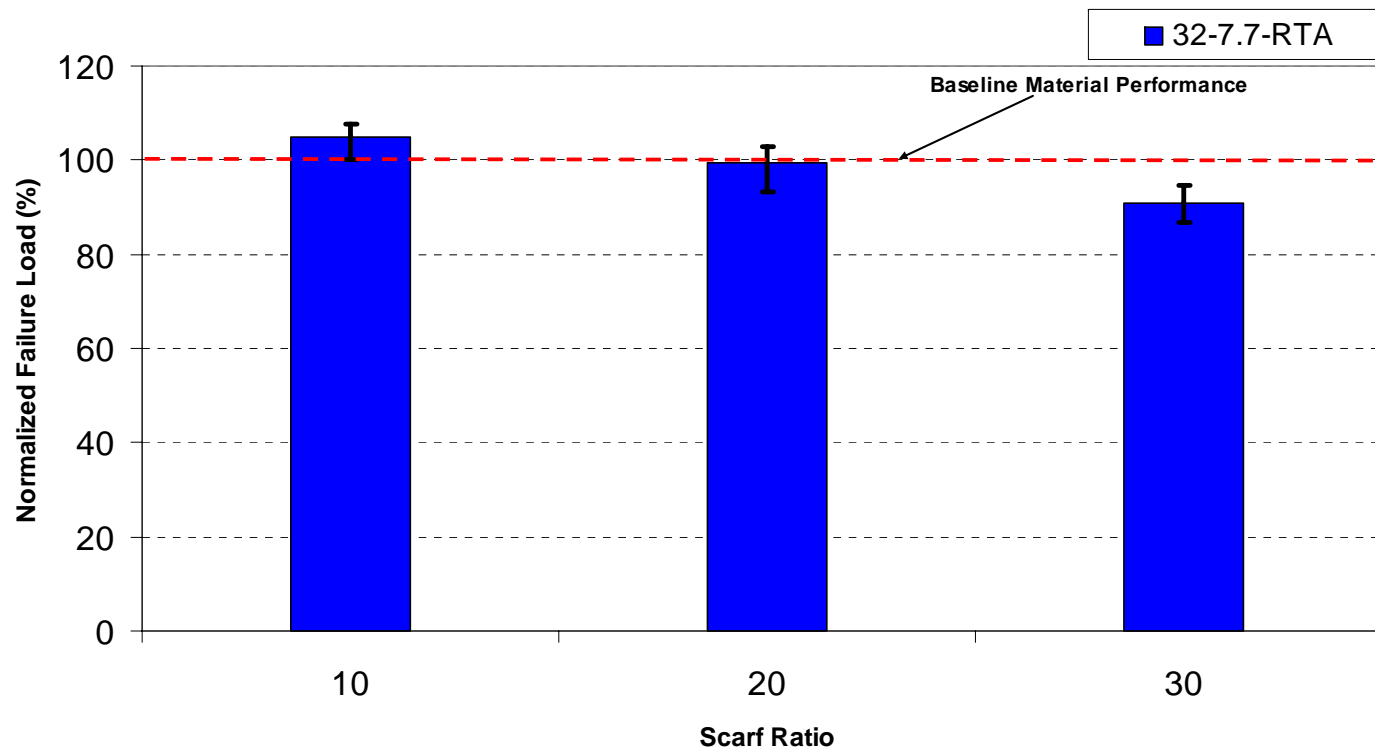


Results-Static

Field Repair Material Evaluation

- Comparison of static strength of the field repairs wrt OEM repairs
- At least 90% “baseline repair performance” was restored at room temperature

Field Repair Material Performance

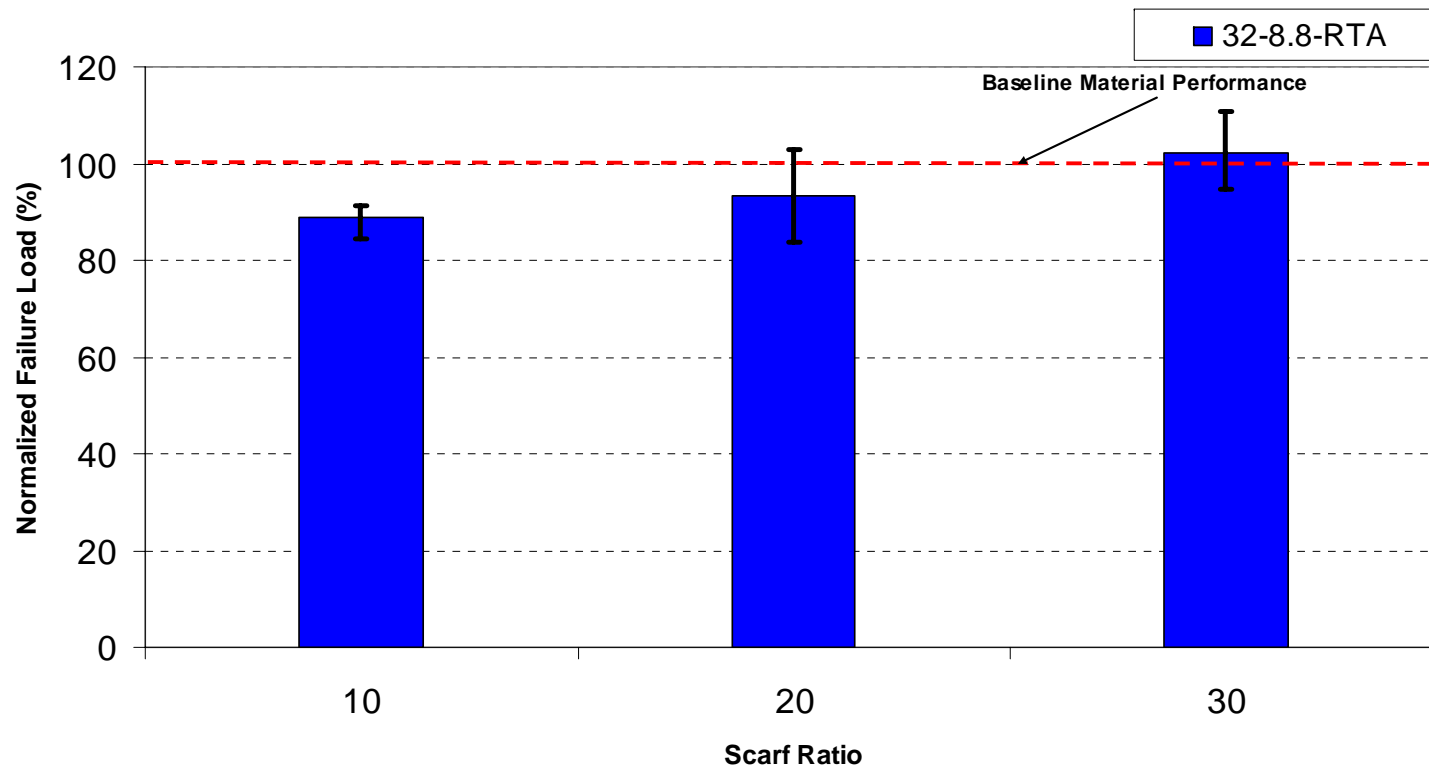


Results-Static

Field Repair Material Evaluation

- Comparison of static strength of the field repairs wrt OEM repairs
- At least 89% “baseline repair performance” was restored at room temperature

Field Repair Material Performance

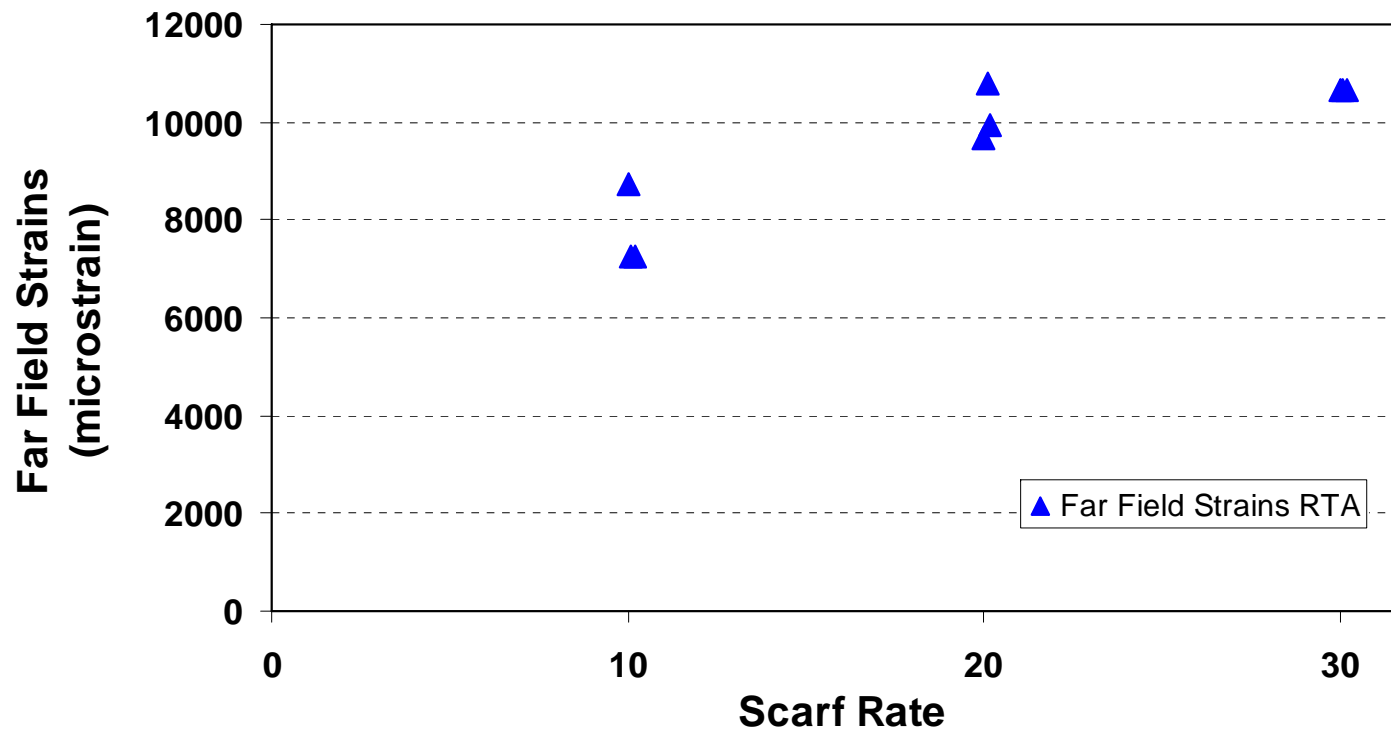


Results-Static

Field Repair Material Evaluation

- Substrate ultimate strain as a function of repair size

Far Field Strains As a Function of Scarf Rate -
ACG MTM45-1 18 ply Panel 1

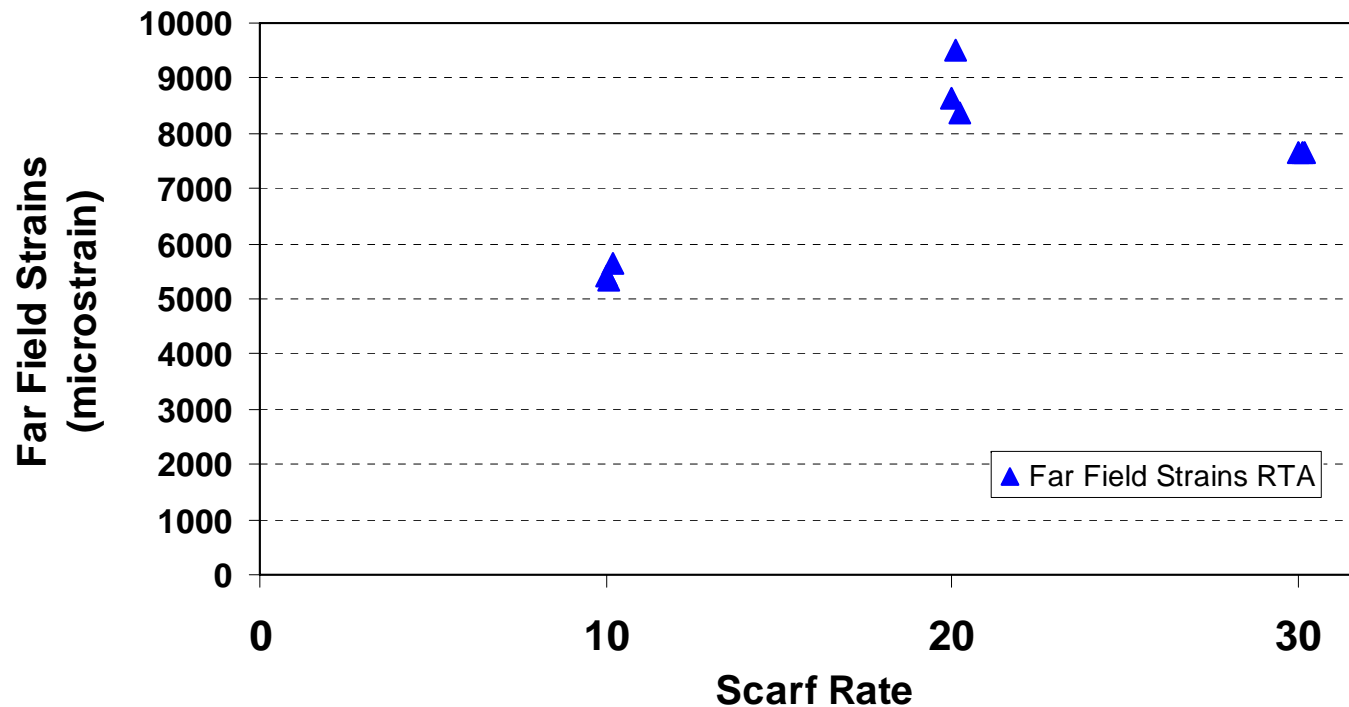


Results-Static

Field Repair Material Evaluation

- Substrate ultimate strain as a function of repair size

Far Field Strains As a Function of Scarf Rate -
ACG MTM45-1 32 ply Panel 6



Methodology - Field Repair Material Evaluation- Summary

- **Field repair material cured at 250°F under vacuum**
- **At least 89% of RTA baseline joint strength was restored for most cases**
- **A few low data points (porosity, process variability)**
- **A higher strength knockdown with respect to baseline repair material performance was observed for CTD and ETW specimens**
- **The thicker specimens 32 ply repairs survived 3DSO in fatigue for all RTD specimens**
- **For the 18 ply repairs, the -30 all survived 3DSO (165000) in fatigue at RTA**

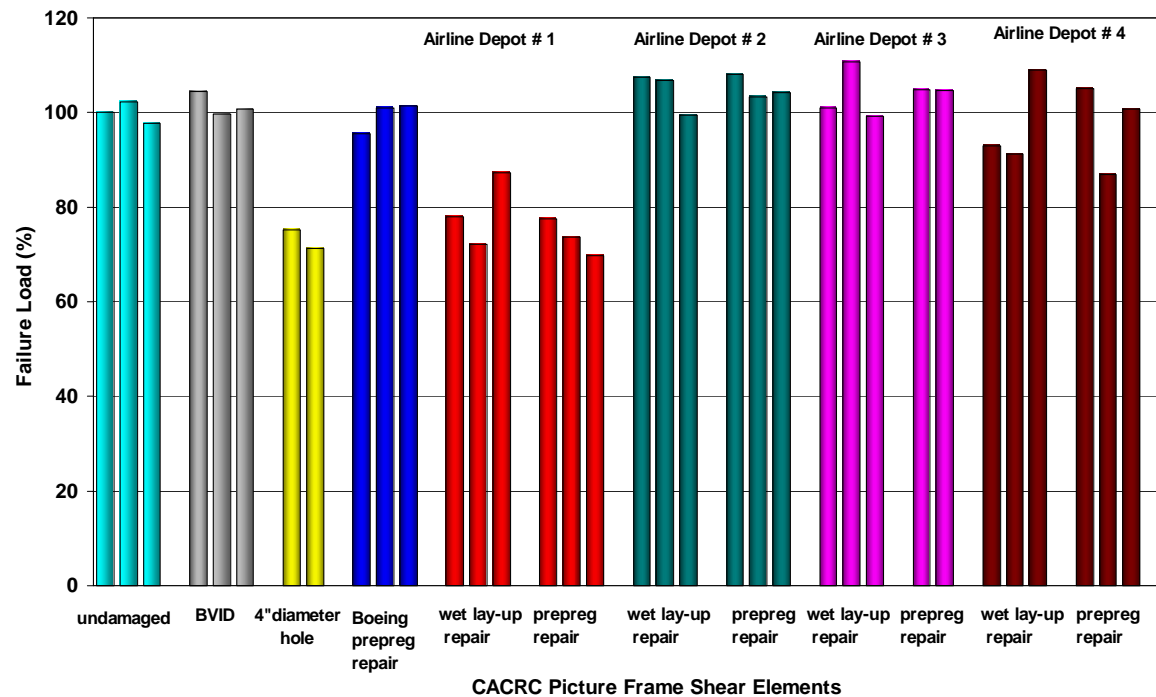
Methodology

Effects of Contamination

- The quality of training and experience of repair technicians is directly associated with the technician's successful implementation of a repair
- Process deviation directly affects the strength of the repair
- Summary of previous FAA/WSU repair study, PFS elements where sent for repair to various airline depots using the same procedures (OEM/ CACRC)

25% strength degradation for repairs performed by airline depot 1

Heat blanket failure



Presented at the CACRC Meeting, November 16th, 2007

Methodology

Effects of Contamination

- To evaluate the strength of contaminated repairs applied to laminate configurations. Five different contaminants are considered: Hydraulic oil (skydrol), jet fuel (JP8), paint stripper, water and perspiration. The effects of each one of the contaminants is being evaluated according to the proposed test matrix. A total of 168 contaminated coupons are being used for this evaluation.

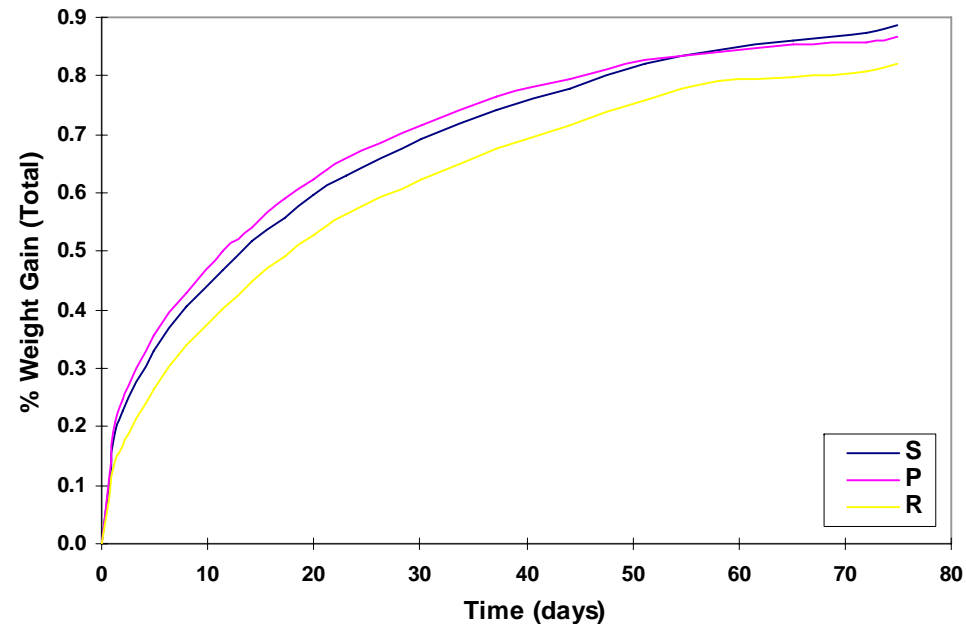
Modulus	scarf rate	Test Condition	Contamination													
			Skydrol		Jet Fuel		Paint Stripper		Water							
									75%		50%		25%		0%	
7.7	10	RTA	3	3	3	3	3	3	3	3	3	3	3	3	3	3
	20	RTA	3	3	3	3	3	3	3	3	3	3	3	3	3	3
8.8	10	RTA	3	3	3	3	3	3	3	3	3	3	3	3	3	3
	20	RTA	3	3	3	3	3	3	3	3	3	3	3	3	3	3

Contamination Test Matrix (Laminate)

Methodology

Effects of Contamination

Contaminant	Minimum Soak Time
Jet Fuel, JP8	30 days
Paint Stripper	6 days
Skydrol	30 days
Water	30 days



After saturation, coupons have been dried to achieve saturation levels of 0%,25%, 50%, 75% and 100%

Methodology

Effects of Contamination

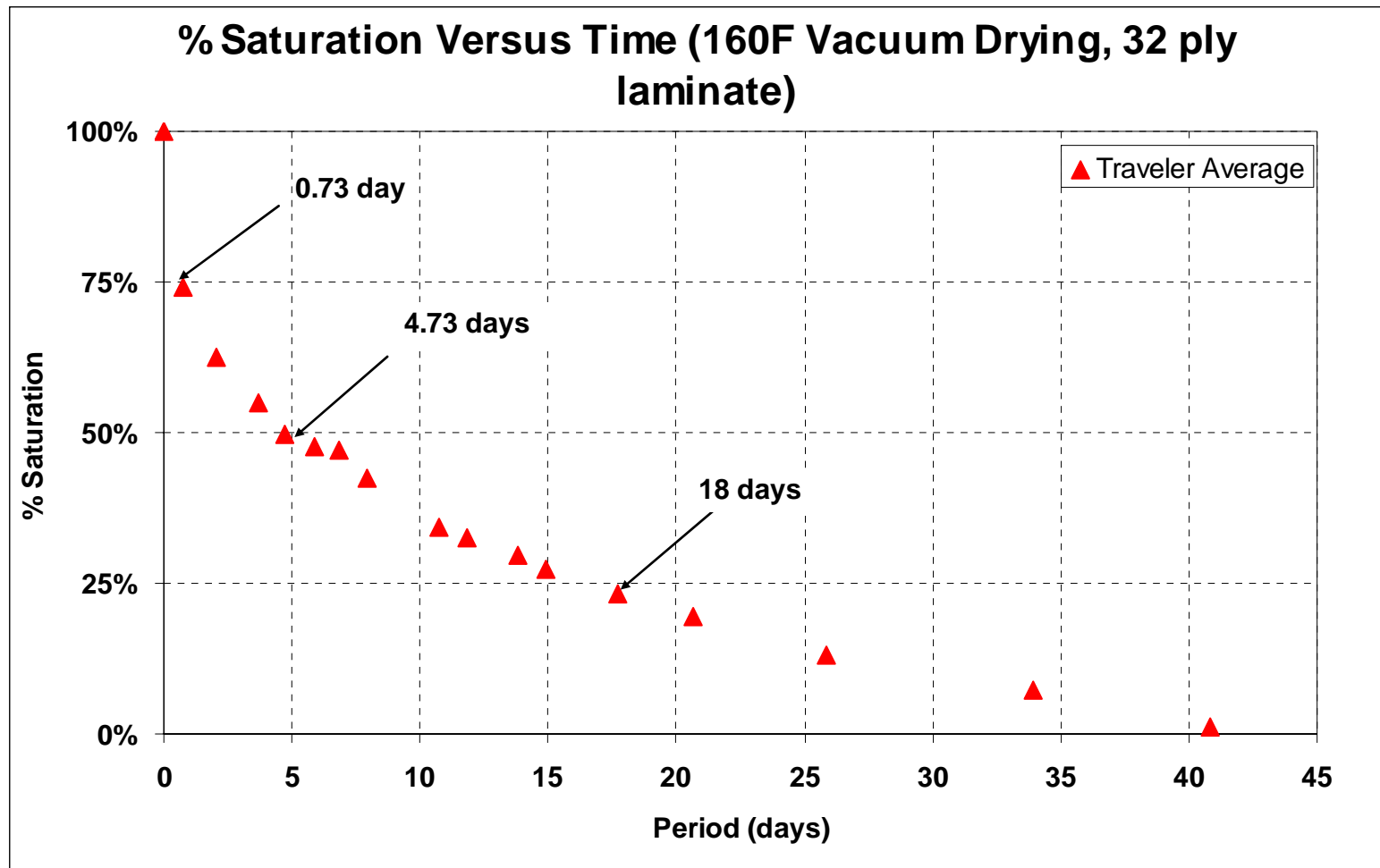


Exposure to Water and Skydrol

Presented at the CACRC Meeting, November 16, 2007

Methodology

Effects of Contamination

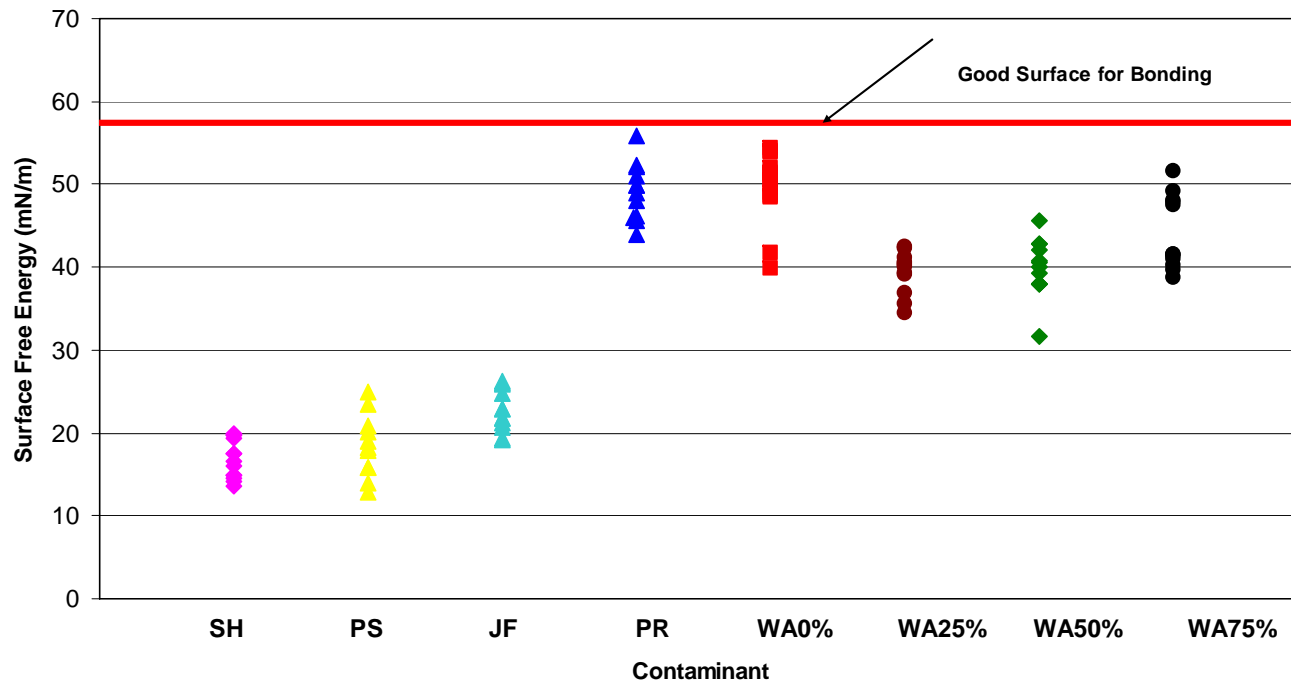


Methodology

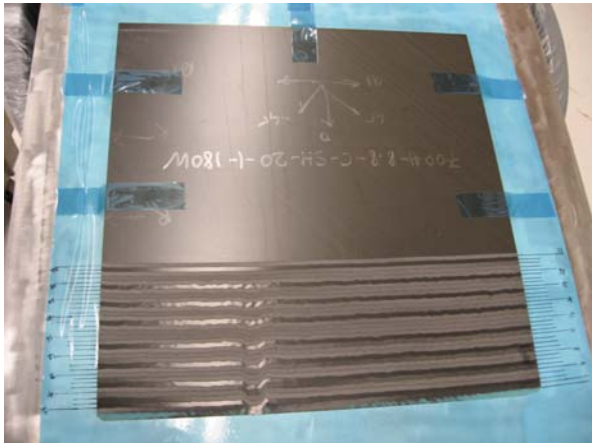
Effects of Contamination

Surface Analysis: Dr Stevenson/ Irish Alcalen

Surface Free Energy Measurements for Contaminated Surfaces prior to Repair



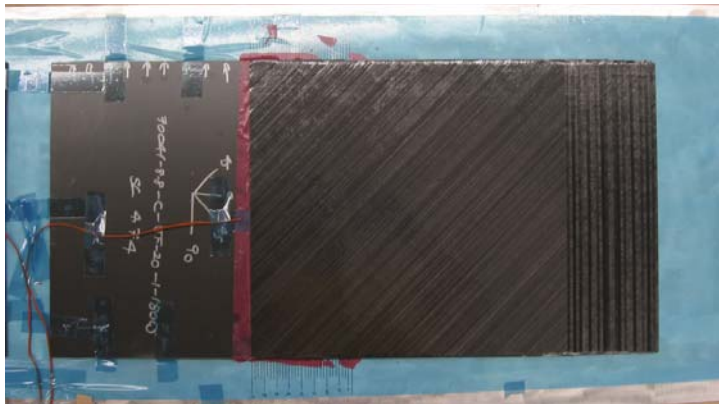
Repair after Contaminant Exposure



Individual Ply Location Marking



Adhesive Application

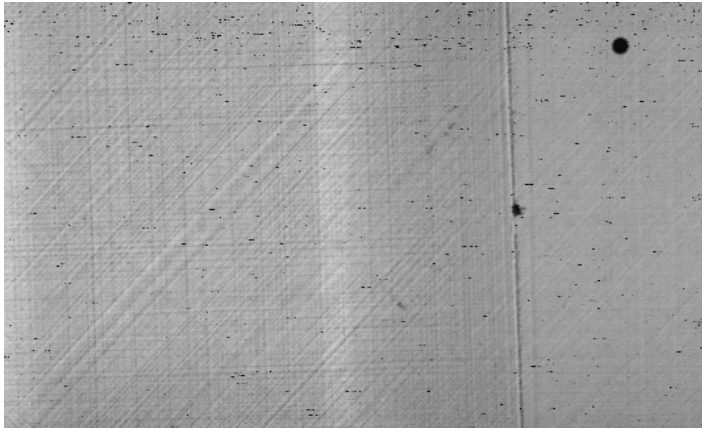


Repair Lay-up/ Thermocouple Installation

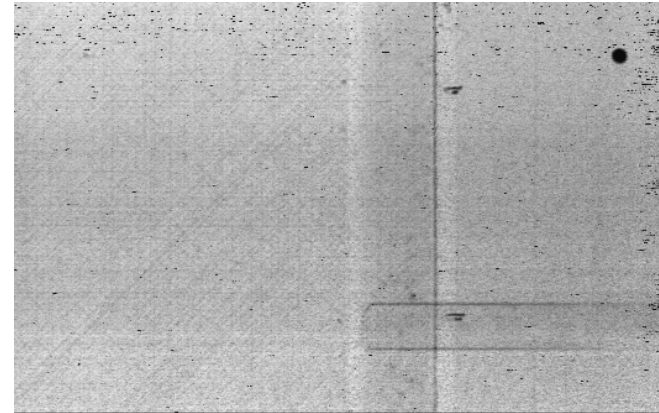


Repair Bagging

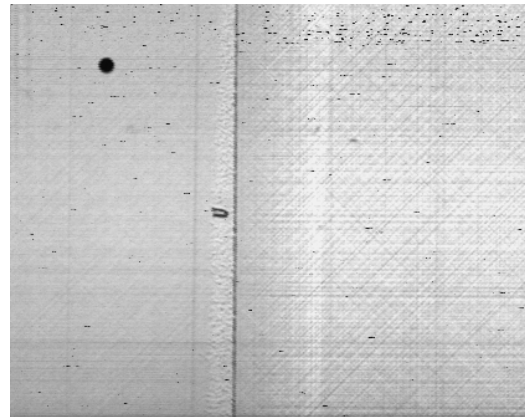
TTU Non-Destructive Inspection



Jet Fuel Contaminated Panel



Skydrol Contaminated Panel

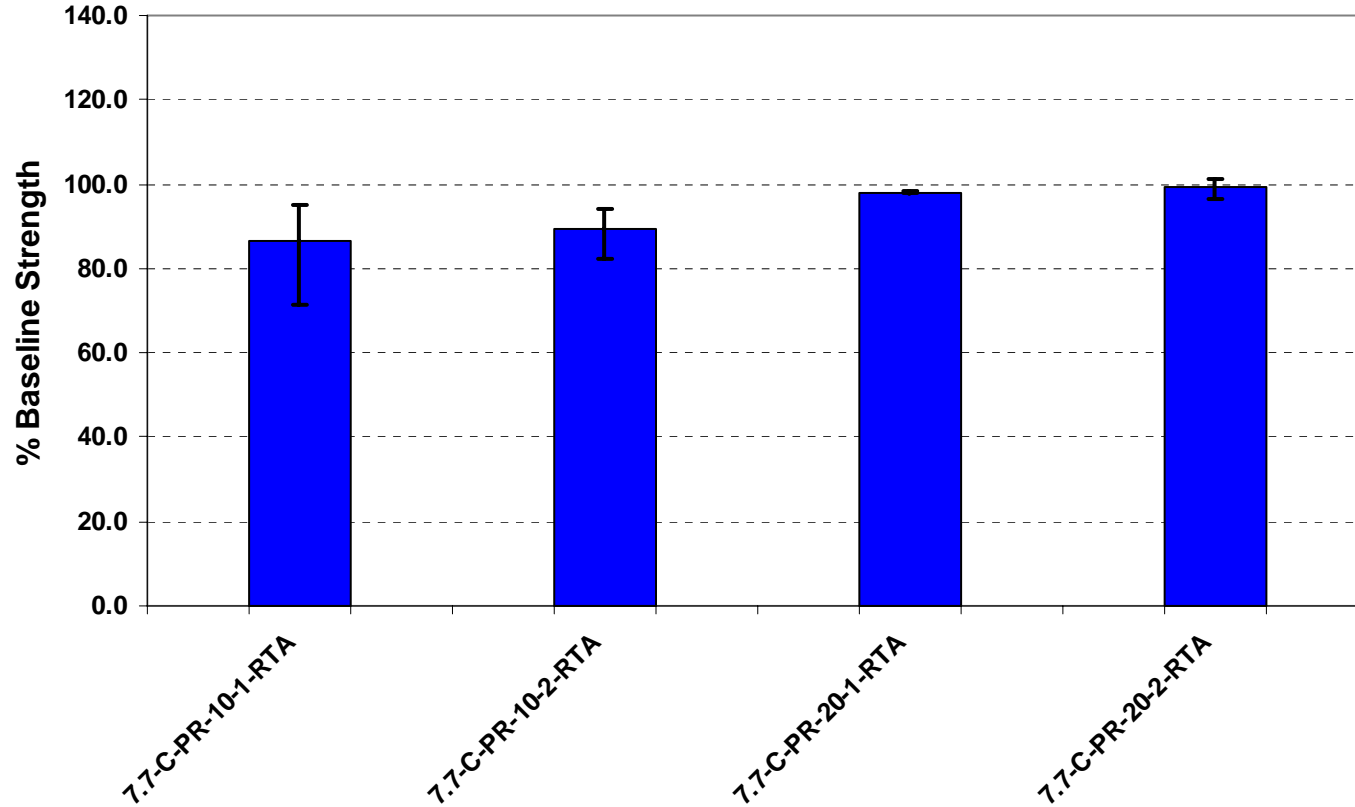


Water Contaminated Panel

Contamination Results

Max Strength degradation 14%

Strength Performance of Coupons Exposed to Perspiration as the Contaminant

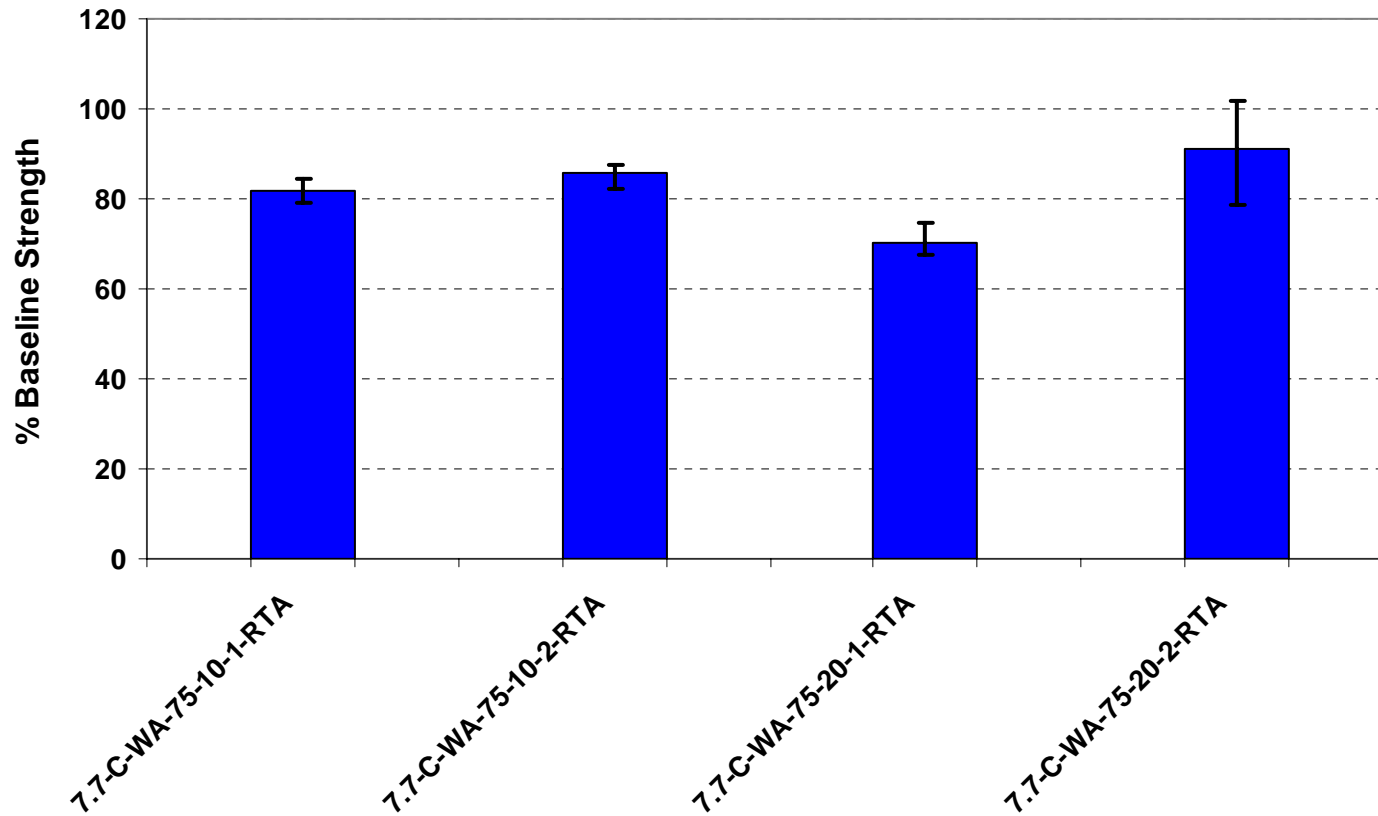


Presented at the CACRC Meeting, November 16th, 2007

Contamination Results

Max Strength degradation 30%

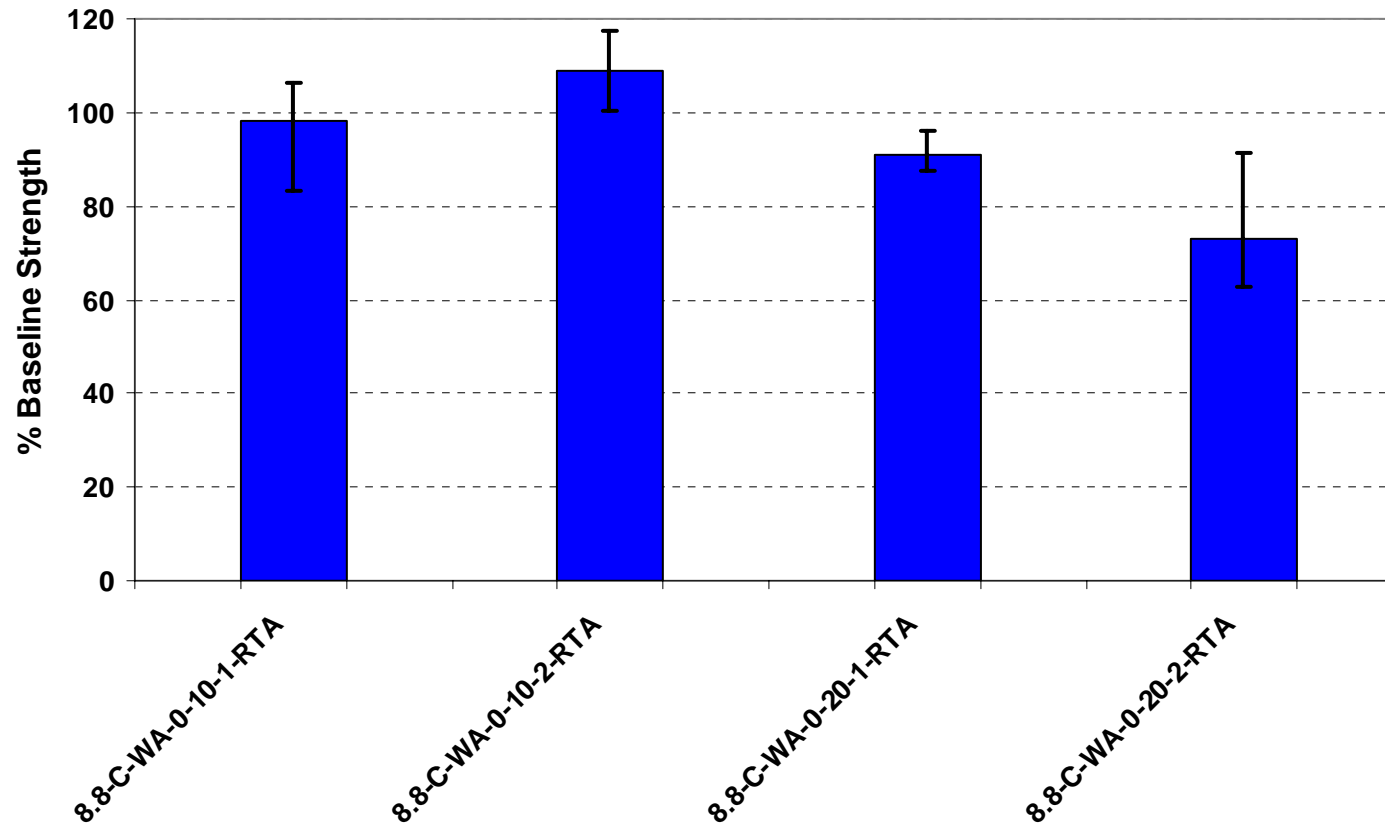
Strength Performance of Coupons Exposed to WA (75% saturation)
as the Contaminant



Contamination Results

Max Strength degradation 27%

Strength Performance of Coupons Exposed to WA (0% moisture after full saturation) as the Contaminant



Presented at the CACRC Meeting, November 16th, 2007

Methodology

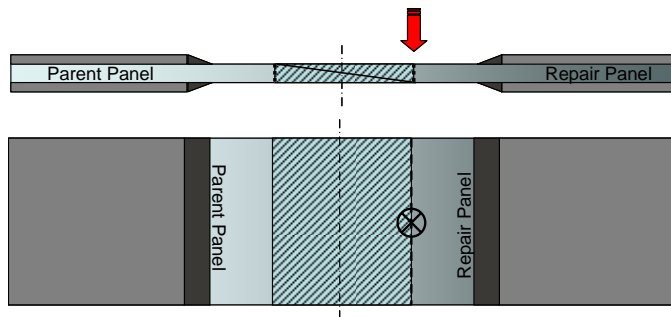
Effects of Contamination

- **Static data showed a lower strength performance for all panels contaminated with PR, WA75%, WA 50%, WA 25%, WA 0%**
- **RTA Static data showed minor strength degradation for panels contaminated with JF, SH and PS**
- **Need fatigue data to confirm results**

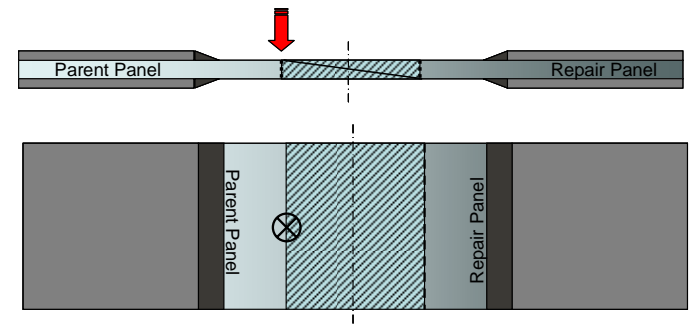
Methodology – Damage Effects

- To evaluate the strength, durability and damage tolerance of repairs applied to laminate structures. 144 Coupons of different thicknesses and stiffnesses are being considered and are being impacted in three different locations: at the center of the repair scarf and at the edge of the scarf.

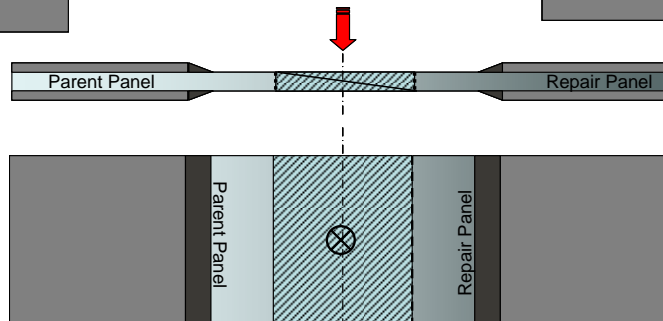
Tip of the scarf far side TF



Tip of the scarf TN



Center Impact



Methodology – Damage Effects

Plies	Modulus	scarf rate	Test Condition	Impact Site		
				TN	TF	CN
18	7.2	10	RTA	3	3	3
			RTF	3	3	3
		20	RTA	3	3	3
			RTF	3	3	3
	9.1	10	RTA	3	3	3
			RTF	3	3	3
		20	RTA	3	3	3
			RTF	3	3	3
48	7.2	10	RTA	3	3	3
			RTF	3	3	3
		20	RTA	3	3	3
			RTF	3	3	3
	9.1	10	RTA	3	3	3
			RTF	3	3	3
		20	RTA	3	3	3
			RTF	3	3	3

18 ply configurations

Impact Energy Level 200 in-lbs

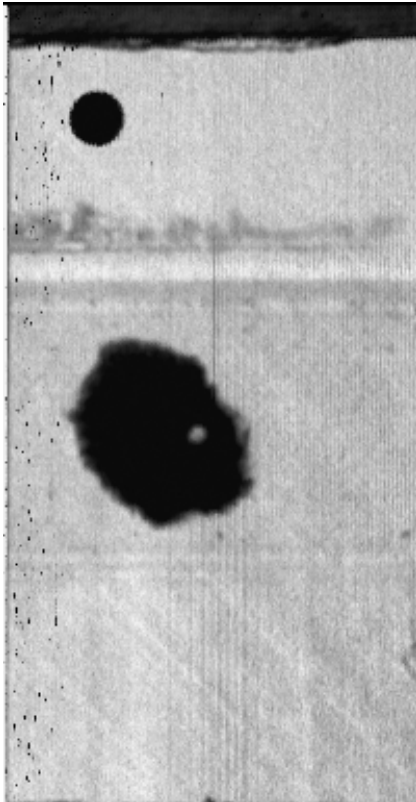
Depth: 0.01”

48 ply configurations

Impact Energy Level 400 in-lbs

Depth: 0.01”

Methodology – Damage Effects



10941-18-7.2-20-CN-180W-1



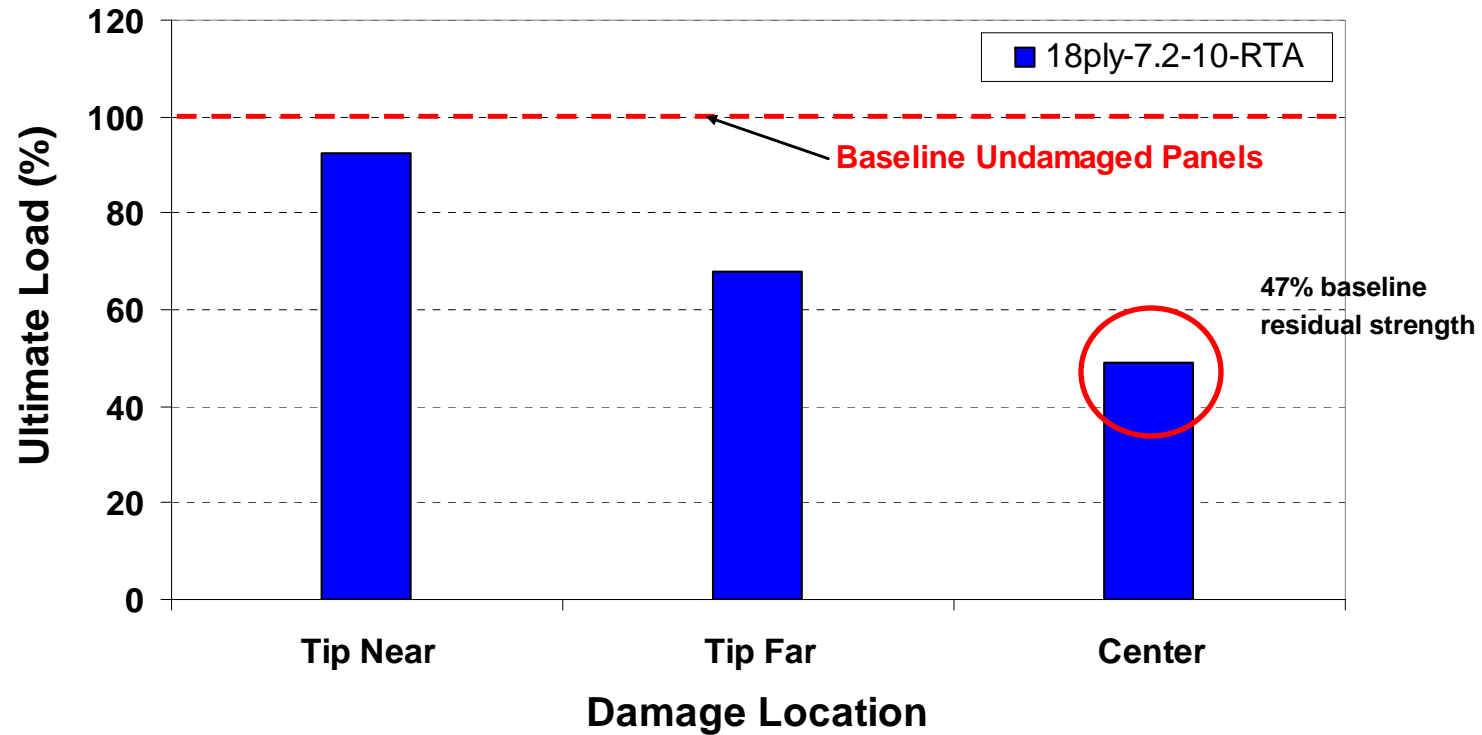
10941-18-7.2-20-CN-180W-2



10941-18-7.2-20-CN-180W-3

Methodology – Damage Effects Results

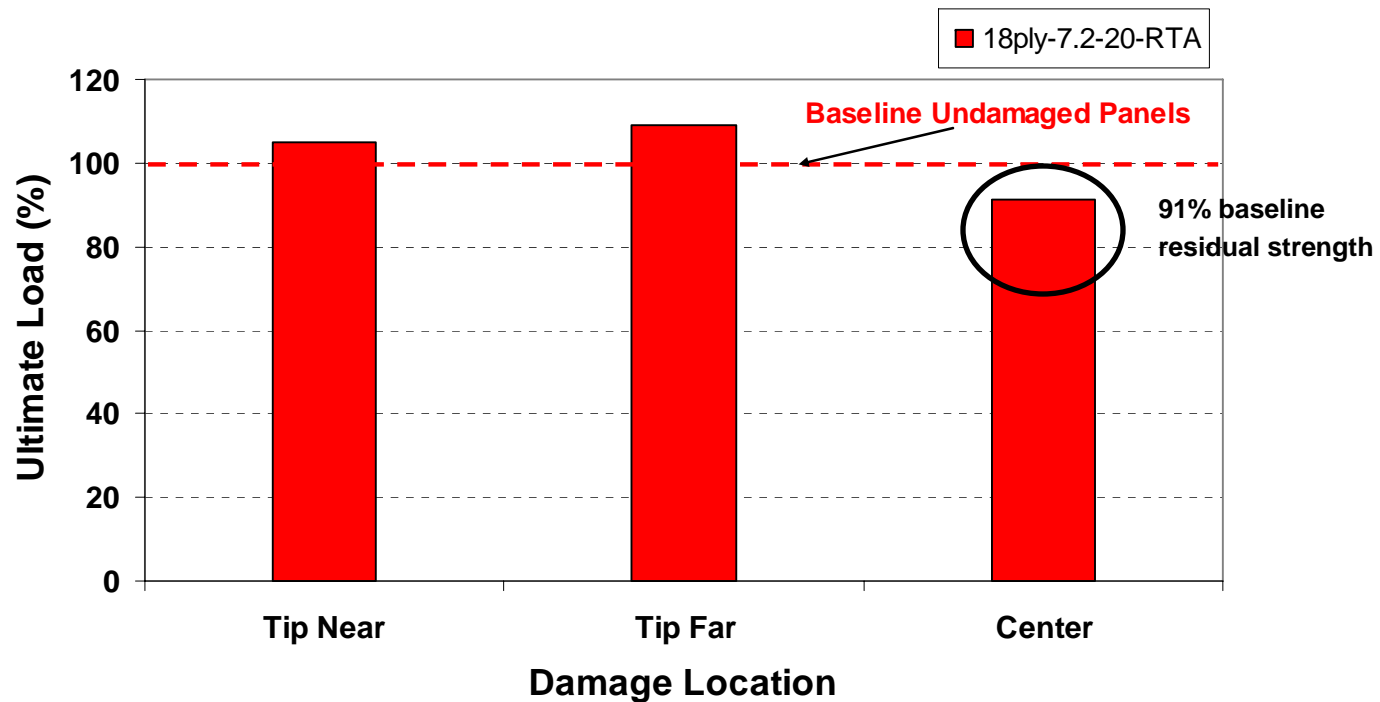
Failure Load, Normalized, as a Function of Damage Location



Methodology – Damage Effects Results

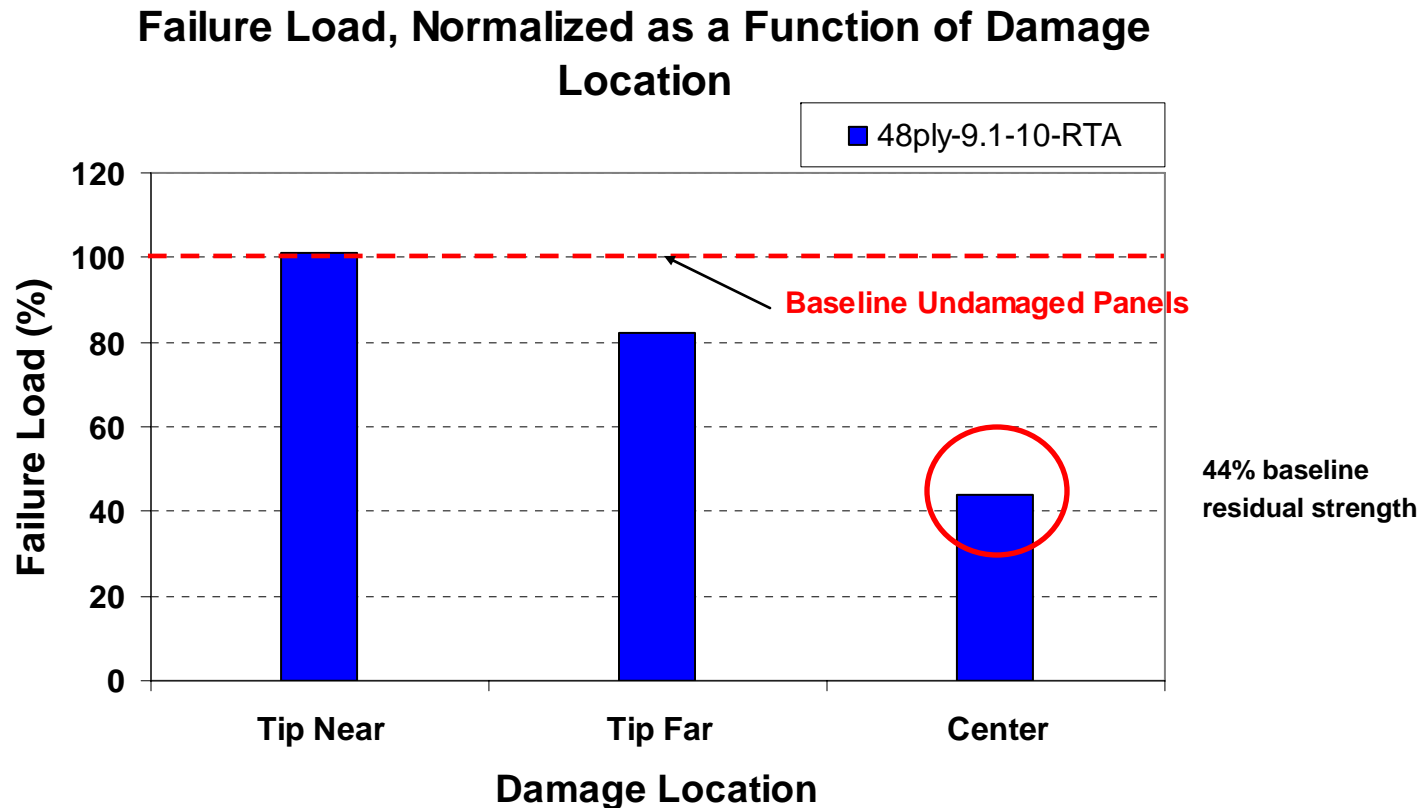
Max Strength Degradation 9%

Failure Load, Normalized as a Function of Damage Location



Presented at the CACRC Meeting, November 16th, 2007

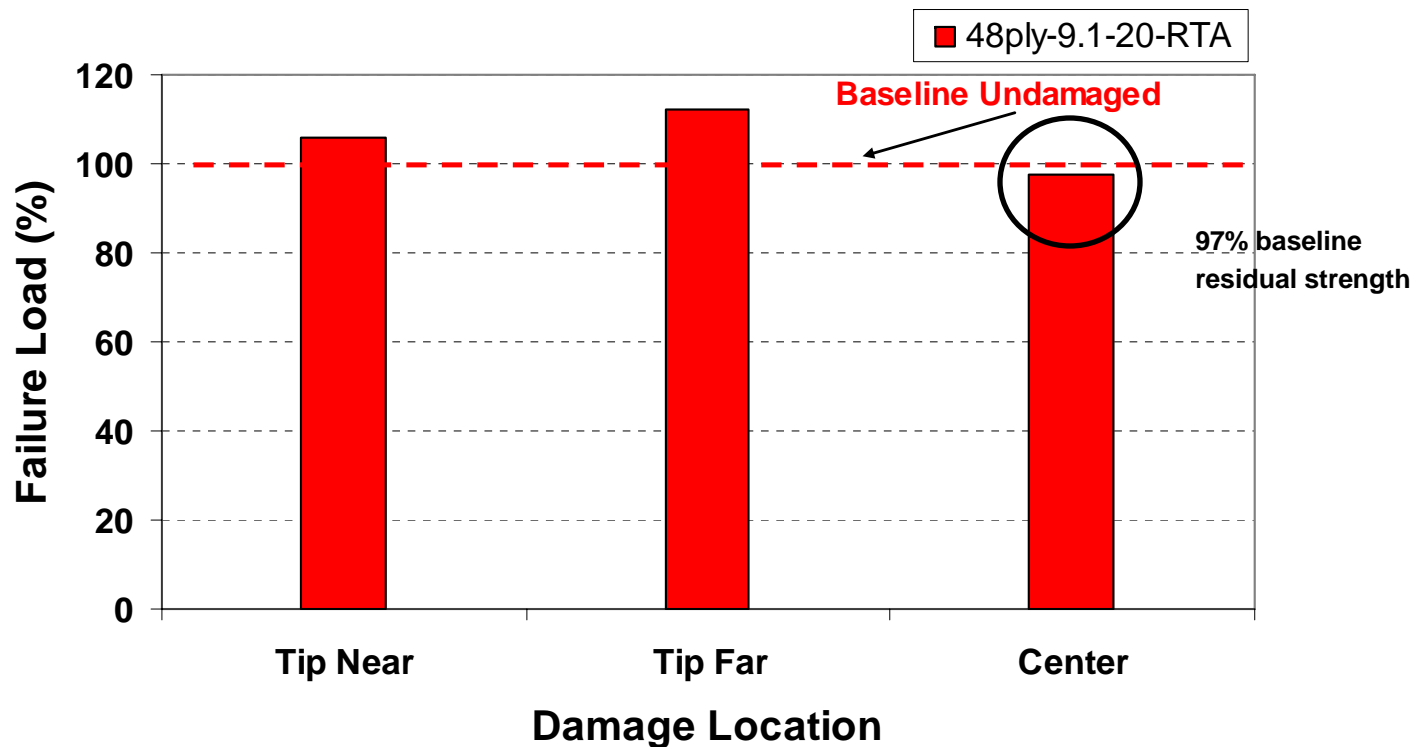
Methodology – Damage Effects Results



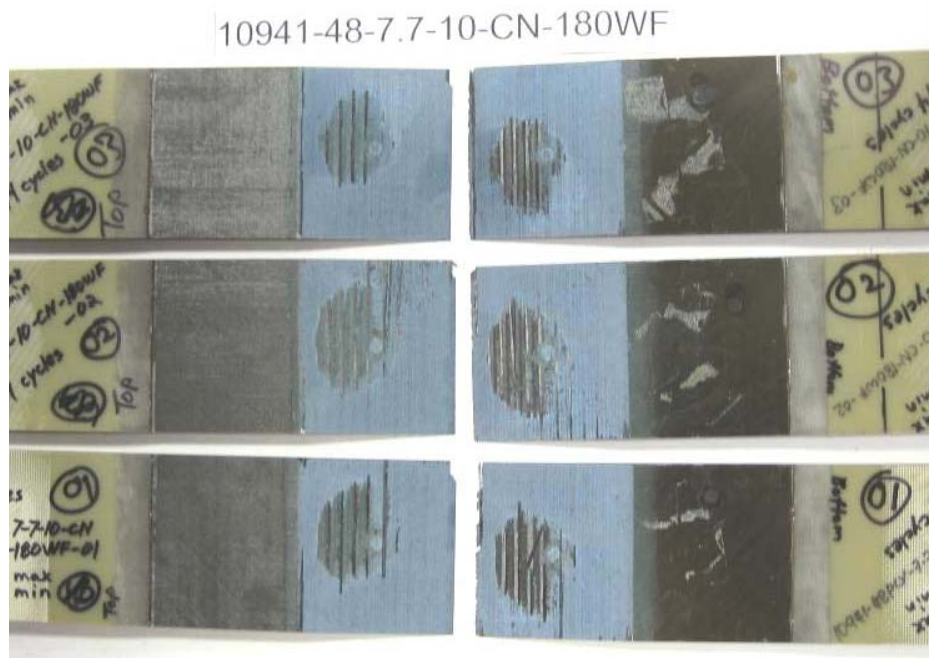
Methodology – Damage Effects Results

Max Strength Degradation 3%

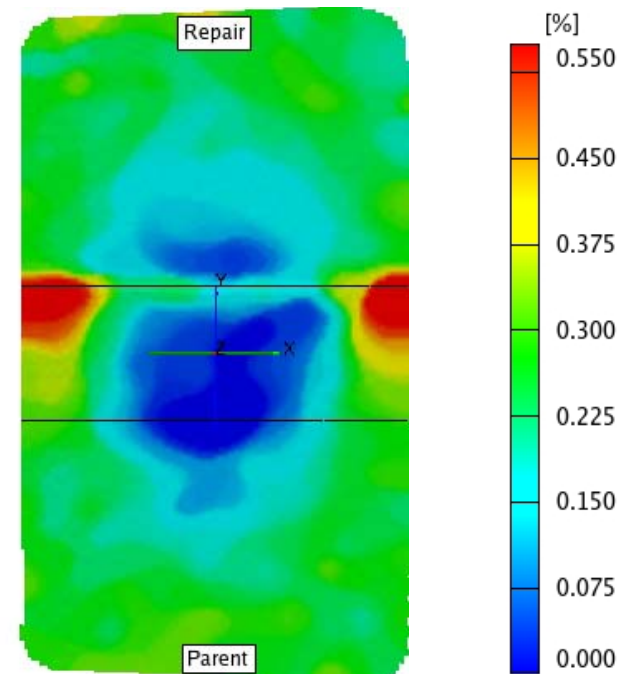
Failure Load, Normalized as a Function of Damage Location



Methodology – Damage Effects Results



Failure Modes (Mainly cohesive)



18-9.1-10-CN-RTA-01 ARAVIS strain Map

Methodology

Damage Effects Summary

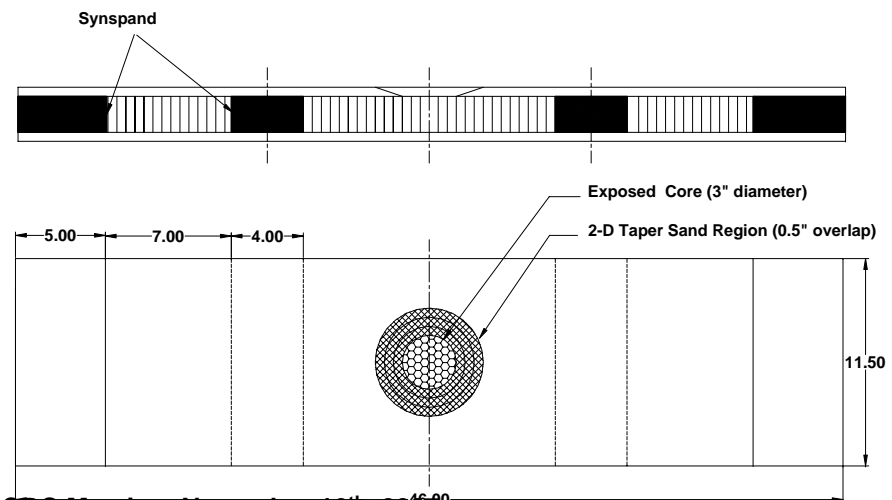
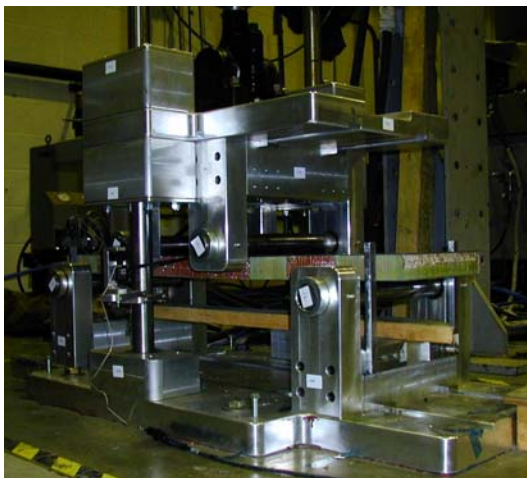
- **Strength degradation is proportional to damage area**
- **Coupons impacted at the center of the repair, had the largest damage area and the lowest static strength**
- **The performance of coupons impacted at the edge of the repair was comparable to that of baseline repaired undamaged coupons**
- **The residual strength is also dependent on the “residual” bond area. The largest repairs are more “damage tolerant” than smaller repairs**

Methodology

Sandwich Repair Evaluation

- To evaluate the strength and durability of OEM vs field repairs. Scarf repairs and external patch repairs are considered for this investigation.

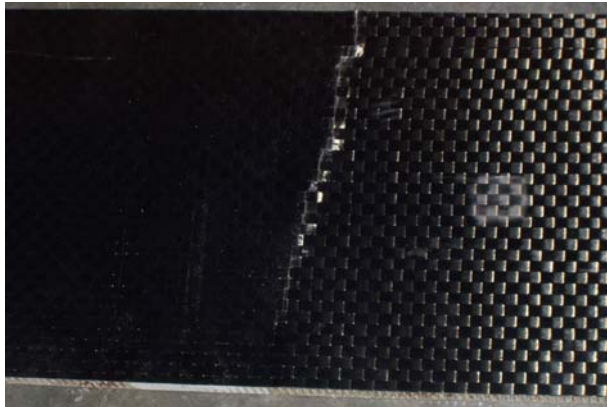
Repair Configuration	Core Cell Size	Repair Material	Repair Type	Scarf Overlap (in)	Static (RTA)	Fatigue (RTA)
2-D Compression Baseline	1/8	Toray T700/2510 PW Prepreg	Baseline Undamaged	NA	6	6
			Flush Scarf Repair	0.5	6	6
			External Patch	0.5	6	6
2-D Compression Baseline	1/8	CACRC Wet Lay-Up Repair	Flush Scarf Repair	0.5	6	6
			External Patch	0.5	6	6
2-D Compression Effects of Cure Cycle Deviations	1/8	CACRC Wet Lay-Up Repair	Flush Scarf Repair/ Undercure	0.5	6	
			Flush Scarf Repair/ Overcure	0.5	6	



Methodology

Sandwich Repair Evaluation

- To evaluate the strength and durability of OEM vs field repairs.



Screening Panels yielded acceptable Failures (9000-10000 microstrain at failure)
Panel Manufacturing and scarfing complete
Repair in progress (OEM)

A Look Forward/ Benefits to Aviation

- **To generate repair data for OEM/ factory materials that can be used to demonstrate acceptability of alternate materials to use for repair when the parent material is not available or cannot be used for repair**
- **To generate data that correlates contamination and process parameter deviation to the performance of bonded repairs**
- **To provide information on repair damage tolerance depending on the area where the damage was inflicted**
- **To identify the crucial steps in bonded repair**
- **To develop rigorous repeatable repair processes that ensure structural integrity of bonded repairs**
- **To gain confidence in bonded structural repairs**